

# Design of bounded feedback controls for linear dynamical systems by using common Lyapunov functions

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**Abstract** For a linear dynamical system, we address the problem of devising a bounded feedback control, which brings the system to the origin in finite time. The construction is based on the notion of a common Lyapunov function. It is shown that the constructed control remains effective in the presence of small perturbations. © 2011 The Chinese Society of Theoretical and Applied Mechanics. [doi:10.1063/2.1101301]

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Consider a linear autonomous dynamical system

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}, \quad \mathbf{x} \in V \subset \mathbf{R}^n, \quad \mathbf{u} \in U \subset \mathbf{R}^m, \quad (1)$$

such that the Kalman controllability condition is met. We want to build a bounded feedback control  $\mathbf{u} = \mathbf{u}(\mathbf{x})$ , which brings an arbitrary state  $\mathbf{x}_0$  to the origin in finite time, provided that  $|\mathbf{x}_0|$  is small enough. In other words, the corresponding phase curves of equation  $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}(\mathbf{x})$  with the initial conditions  $\mathbf{x}(0) = \mathbf{x}_0$  gets to 0 in finite time. Note that, given a bound  $|\mathbf{u}| \leq C$  on control, it is generally impossible to steer any given initial state into the origin.

The problem of feedback control design has been studied, in particular, by V. Korobov,<sup>[1]</sup> and his paper is a starting point for ours, though our arguments can be hardly put into a direct comparison with that of Ref. [1]. In principle, to get to the zero one can fix the bound  $|\mathbf{u}| \leq C$ , and use the minimum time control  $\mathbf{u}_{\min}$ .<sup>[2,3]</sup> The obvious drawback of this approach consists in the great difficulties of implementation: the amount of computations required is prohibitive for a numerical simulation. Therefore we need the feedback control to be devised in such a way as to be easily implementable (constructive). One can see *a posteriori* that our control algorithm does not require much memory or computational power. To implement it one needs just basic operations of linear algebra plus finding the only root of a scalar monotone function of one variable. Our control is more smooth than the minimum-time one: its only singular point is zero, while the singular locus of optimal control is a singular hypersurface. Moreover, the time  $\tau(\mathbf{x})$  required for our control to bring a given state  $\mathbf{x}$  to 0 is not much greater than the minimal one  $\tau_{\min}(\mathbf{x})$ : the ratio  $\tau(\mathbf{x})/\tau_{\min}(\mathbf{x})$  is bounded as  $\mathbf{x}$  runs over a neighborhood of zero. In our terminology, the feedback control  $\mathbf{u}$  is locally equivalent to the minimum-time control  $\mathbf{u}_{\min}$ .

First, we simplify our control system (1). Note that the feedback control problem does not change essentially under transformation  $\mathbf{A} \mapsto \mathbf{A} + \mathbf{B}\mathbf{C}$ ,  $\mathbf{u} \mapsto \mathbf{u} - \mathbf{C}\mathbf{x}$ , of (1) corresponding to an extra linear feedback. Moreover, for any invertible matrix  $\mathbf{D}$  the gauge

transformation  $\mathbf{A} \mapsto \mathbf{D}^{-1}\mathbf{A}\mathbf{D}$ ,  $\mathbf{B} \mapsto \mathbf{D}^{-1}\mathbf{B}$ ,  $\mathbf{u} \mapsto \mathbf{u}$  does not affect the problem. By using these transformations one can bring system (1) to the canonical Brunovsky form<sup>[4–6]</sup> — a set of independent subsystems of the form  $\dot{z}^{(k)} = u; z, u \in \mathbf{R}^1$ . Now it suffices to bring each subsystem  $\dot{z}^{(k)} = u$  to zero by a bounded feedback control.

Thus, the general problem (1) reduces to the case

$$\mathbf{A} = \begin{pmatrix} 0 & 1 & & \\ & 0 & \ddots & \\ & & \ddots & 1 \\ & & & 0 \end{pmatrix}, \quad \mathbf{B} = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ 1 \end{pmatrix}. \quad (2)$$

We introduce a scalar function  $T = T(\mathbf{x})$  which is specified below. System (1), (2) is related to a distinguished function matrix

$$\delta(T) = \text{diag}(T^{-n}, T^{-n+1}, \dots, T^{-1})$$

such that

$$\delta \mathbf{A} \delta^{-1} = T^{-1} \mathbf{A}, \quad \delta \mathbf{B} = T^{-1} \mathbf{B}, \quad \frac{d}{dT} \delta = T^{-1} \mathbf{M} \delta, \quad (3)$$

where  $\mathbf{M} = -\text{diag}(n, n-1, \dots, 1)$ . This implies immediately that for  $\mathbf{y} = \delta \mathbf{x}$  we have

$$\dot{\mathbf{y}} = T^{-1} (\mathbf{A}\mathbf{y} + \mathbf{B}\mathbf{u} + \dot{T} \mathbf{M} \mathbf{y}). \quad (4)$$

Here we present the main novelty of the paper: a construction of a common Lyapunov function for two specific stable matrices. Our feedback controls are based on the existence of this function.

In notations (2) consider stable matrices  $\tilde{\mathbf{A}}$  of the form

$$\tilde{\mathbf{A}} = \mathbf{A} + \mathbf{B}\mathbf{C}, \quad (5)$$

where the row-vector  $\mathbf{C} = (c_1, \dots, c_n)$  is regarded as a  $1 \times n$  matrix. In other words,

$$\tilde{\mathbf{A}} = \begin{pmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 1 \\ c_1 & c_2 & c_3 & \dots & c_n \end{pmatrix},$$

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and the polynomial  $f(x) = x^n - \sum_{i=1}^n c_i x^{i-1}$  is stable, i.e. all its roots have a negative real part.

**Theorem 1** One can choose the vector  $\mathbf{C}$  in such a way that the stable matrices  $\tilde{\mathbf{A}}$  and  $\mathbf{M}$  possess a common quadratic Lyapunov function: There exist symmetric positive definite matrices  $\mathbf{Q}$ ,  $\mathbf{P}$ , and  $\mathbf{R}$  such that

$$\mathbf{Q}\tilde{\mathbf{A}} + \tilde{\mathbf{A}}^* \mathbf{Q} = -\mathbf{P}, \quad \mathbf{Q}\mathbf{M} + \mathbf{M}\mathbf{Q} = -\mathbf{R} \quad (6)$$

**Remark.** The vector  $\mathbf{C}$  can be defined as follows Put

$$f_\lambda(x) = \prod_{k=1}^n (x + e^{\lambda k}) = x^n - \sum_{i=1}^n c_i x^{i-1}.$$

Then  $\mathbf{C}$  fits the theorem, provided that  $\lambda > 0$  is large enough.

Now we can define a bounded feedback control  $u$  which brings the system (1), (2) to zero in finite time. Put  $\mathbf{y} = \delta(T)\mathbf{x}$ ,  $\mathbf{u}(\mathbf{x}) = (\mathbf{C}, \mathbf{y})$ , where (the row-vector)  $\mathbf{C}$  is chosen in Theorem 1. We define the function  $T$  by  $T(0) = 0$  and

$$(\mathbf{Q}\mathbf{y}, \mathbf{y}) = 1, \text{ where } \mathbf{y} = \delta(T)\mathbf{x} \text{ if } \mathbf{x} \neq 0. \quad (7)$$

The definition is correct, since for a fixed  $\mathbf{x} \neq 0$  the analytic function  $\phi(T) = (\mathbf{Q}\delta(T)\mathbf{x}, \delta(T)\mathbf{x})$  decreases as  $T$  increases, and tends to infinity as  $T \rightarrow 0$ , and to zero as  $T \rightarrow \infty$ . Indeed, by virtue of Theorem 1

$$\frac{d}{dT}\phi(T) = T^{-1}((\mathbf{Q}\mathbf{M} + \mathbf{M}\mathbf{Q})\mathbf{y}, \mathbf{y}) < 0 \quad (8)$$

Moreover,  $T$  depends on  $\mathbf{x}$  analytically if  $\mathbf{x} \neq 0$ , and the condition (7) guarantee the boundedness of  $\mathbf{u}(\mathbf{x}) = (\mathbf{C}, \mathbf{y}(\mathbf{x}))$ .

Now it follows from Eqs. (7) and (4) that

$$(\mathbf{y}, (\mathbf{Q}\tilde{\mathbf{A}} + \tilde{\mathbf{A}}^* \mathbf{Q})\mathbf{y} + \dot{T}(\mathbf{Q}\mathbf{M} + \mathbf{M}\mathbf{Q})\mathbf{y}) = 0,$$

or

$$\dot{T} = -\frac{(\mathbf{y}, (\mathbf{Q}\tilde{\mathbf{A}} + \tilde{\mathbf{A}}^* \mathbf{Q})\mathbf{y})}{(\mathbf{y}, (\mathbf{Q}\mathbf{M} + \mathbf{M}\mathbf{Q})\mathbf{y})}.$$

In view of the Lyapunov equations (6)

$$\dot{T} \leq -c,$$

where  $c = c(\mathbf{Q})$  is a positive constant. This implies that up to the zero  $T$  decreases with a speed separated from 0. Therefore, the motion ends in the zero in finite time  $\tau(\mathbf{x})$  which can be estimated as  $\tau(\mathbf{x}) = O(T(\mathbf{x}))$ . In its turn,  $T(\mathbf{x})$  can be estimated as  $O(\tau_{\min}(\mathbf{x}))$  so that the time required for getting into zero is of the same order of magnitude as the minimal one. The result of this section can be stated as follows:

**Theorem 2** Suppose  $\mathbf{Q}(\mathbf{x}) = (\mathbf{Q}\mathbf{x}, \mathbf{x})$  is a common quadratic Lyapunov function for two stable matrices  $\tilde{\mathbf{A}} = \mathbf{A} + \mathbf{B}\mathbf{C}$  and  $\mathbf{M}$ . Then, condition (7) defines a bounded feedback control  $\mathbf{u}(\mathbf{x}) = (\mathbf{C}, \mathbf{y}(\mathbf{x})) = (\mathbf{C}, \delta(T(\mathbf{x}))\mathbf{x})$  bringing any state vector of system (1), (2) to zero in finite time. This time has the same order of magnitude as the minimal one.

**Remark.** Note that the proposed control is global: it is bounded in the whole phase space and brings any initial state of system (1), (2) to zero in finite time. It also remains effective for the system

$$z^{(n)} = u + v$$

under small perturbation  $\mathbf{v}$ .

One can generalize the above first method of control as follows: We again put  $\mathbf{y} = \delta(T)\mathbf{x}$ ,  $\mathbf{u}(\mathbf{x}) = (\mathbf{C}, \mathbf{y})$ , but define the function  $T$  by condition

$$T^{-2\beta}(\mathbf{Q}\mathbf{y}, \mathbf{y}) = 1, \quad (9)$$

where  $\beta \geq 0$  is a new parameter. Introduction of the new parameter does not spoil our previous arguments essentially. The function  $\phi_\beta(T) = T^{-2\beta}(\mathbf{Q}\delta(T)\mathbf{x}, \delta(T)\mathbf{x})$  tends to infinity as  $T \rightarrow 0$ , and to zero as  $T \rightarrow \infty$ . Moreover,

$$\frac{d}{dT}\phi_\beta(T) = T^{-1-2\beta}((\mathbf{Q}\mathbf{M}_\beta + \mathbf{M}_\beta \mathbf{Q})\mathbf{y}, \mathbf{y}), \quad (10)$$

where  $\mathbf{M}_\beta = \mathbf{M} - \beta\mathbf{I}$ . If the matrix  $\mathbf{Q}$  defines a quadratic Lyapunov function for the stable matrix  $\mathbf{M}_\beta$ , then we see from (10) that  $\phi_\beta(T)$  decreases as  $T$  increases. This allows us to define the function  $T = T(\mathbf{x})$ . Similarly to our arguments in the previous section it follows from Eqs. (9) and (4) that

$$\dot{T} = -\frac{(\mathbf{y}, (\mathbf{Q}\tilde{\mathbf{A}} + \tilde{\mathbf{A}}^* \mathbf{Q})\mathbf{y})}{(\mathbf{y}, (\mathbf{Q}\mathbf{M}_\beta + \mathbf{M}_\beta \mathbf{Q})\mathbf{y})}. \quad (11)$$

If the matrix  $\mathbf{Q}$  defines a common quadratic Lyapunov function for two stable matrices  $\tilde{\mathbf{A}} = \mathbf{A} + \mathbf{B}\mathbf{C}$  and  $\mathbf{M}_\beta = \mathbf{M} - \beta\mathbf{I}$  then the above arguments prove that the controlled motion ends in the zero in finite time  $\tau(\mathbf{x}) = O(T(\mathbf{x}))$ .

The result of this section can be stated as follows:

**Theorem 3** Suppose  $\mathbf{Q}(\mathbf{x}) = (\mathbf{Q}\mathbf{x}, \mathbf{x})$  is a common quadratic Lyapunov function for two stable matrices  $\tilde{\mathbf{A}} = \mathbf{A} + \mathbf{B}\mathbf{C}$  and  $\mathbf{M}_\beta = \mathbf{M} - \beta\mathbf{I}$ . Then, condition (9) defines a bounded feedback control  $\mathbf{u}(\mathbf{x}) = (\mathbf{C}, \mathbf{y}(\mathbf{x})) = (\mathbf{C}, \delta(T(\mathbf{x}))\mathbf{x})$  bringing any state vector of the system (1),(2) to zero in finite time.

**Remark.** Note that Theorem 2 is based on a rather deep Theorem 1. On the contrary, conditions of Theorem 3 can be easily verified in many cases, e.g. if  $\beta$  is large, without appealing to any deep result. On the other hand, the time for getting to zero needed by Theorem 3 can be much greater than that in Theorem 2.

The second method of control has an advantage in that it still works under smooth perturbations

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{f}(\mathbf{x}) + \mathbf{B}u, \quad \mathbf{f}(\mathbf{x}) = O(|\mathbf{x}|^2) \quad (12)$$

of the control system.

**Theorem 4** Suppose  $\mathbf{Q}(\mathbf{x}) = (\mathbf{Q}\mathbf{x}, \mathbf{x})$  is a common quadratic Lyapunov function for two stable matrices  $\hat{\mathbf{A}} = \mathbf{A} + \mathbf{B}\mathbf{C}$  and  $\mathbf{M}_\beta = \mathbf{M} - \beta\mathbf{I}$ , and  $\beta > n - 3$ . Then, condition (9) defines a bounded feedback control  $u(\mathbf{x}) = (\mathbf{C}, \mathbf{y}(\mathbf{x})) = (\mathbf{C}, \delta(T(\mathbf{x}))\mathbf{x})$  bringing any state vector close to zero of the system (12), (2) to zero in finite time.

**Remark.** Thus, the second approach is locally applicable to a nonlinear control system

$$\dot{\mathbf{x}} = \mathbf{F}(\mathbf{x}) + \mathbf{B}u, \quad \mathbf{F}(\mathbf{x}) \in \mathcal{C}^2$$

which can be represented in the form (12) in the vicinity of an equilibrium state.

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